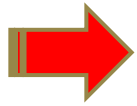


TCAD Simulation of LTPS Hot Carrier Injection Degradation



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Hydrodynamic model for hot carriers:

$$\nabla \cdot S + R_n w - \nabla E_c \cdot J_n + \frac{n(w - w_0)}{\tau_w} + \frac{\partial(nw)}{\partial t} = 0$$

$$S = -\frac{5}{3} J_n w - \frac{10}{9} \mu_n n w \nabla w.$$

where w is the total energy of an electron and $w_0 = 3kT/2$ is the electron energy at equilibrium. S is the electron energy flux intensity and τ_w is the energy relaxation time.

E.M. Azoff. Energy transport numerical simulation of graded AlGaAs/GaAs heterojunction bipolar transistors. *IEEE Trans. ED*, 36(4):609–616, 1989. [doi:10.1109/16.22464](https://doi.org/10.1109/16.22464).

E.M. Azoff. Close-form method for solving the steady-state generalised energy-momentum conservation equations. *COMPEL*, 6(1):25–30, 1987. [doi:10.1108/eb010297](https://doi.org/10.1108/eb010297).

HCI Theory:

Gate injection:

$$j_{\text{HCI}} = q \cdot v_{\text{therm}}(\text{Te}) \cdot n_{\text{channel}} \cdot \text{prob}(\text{Te})$$

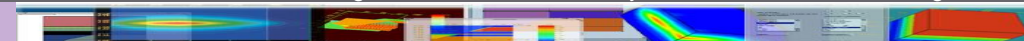
where v_{therm} is the carrier temperature (Te) dependent thermal velocity given by

$$v_{\text{therm}} = \sqrt{k \cdot \text{Te} / (2 \cdot m \cdot \pi)}$$

$\text{prob}(\text{Te})$ is the probability of carriers with temperature higher than Te from TCAD simulation.

To calculate $\text{prob}(\text{Te})$, we assume Boltzman statistics due to the lack of quantum confinement for high energy hot carriers:

$$\text{prob}(\text{Te}) = \sum_{\text{over } k_y \text{ for } E > E_{\text{ox}}} [B \exp(-(E - E_c) / k\text{Te})]$$



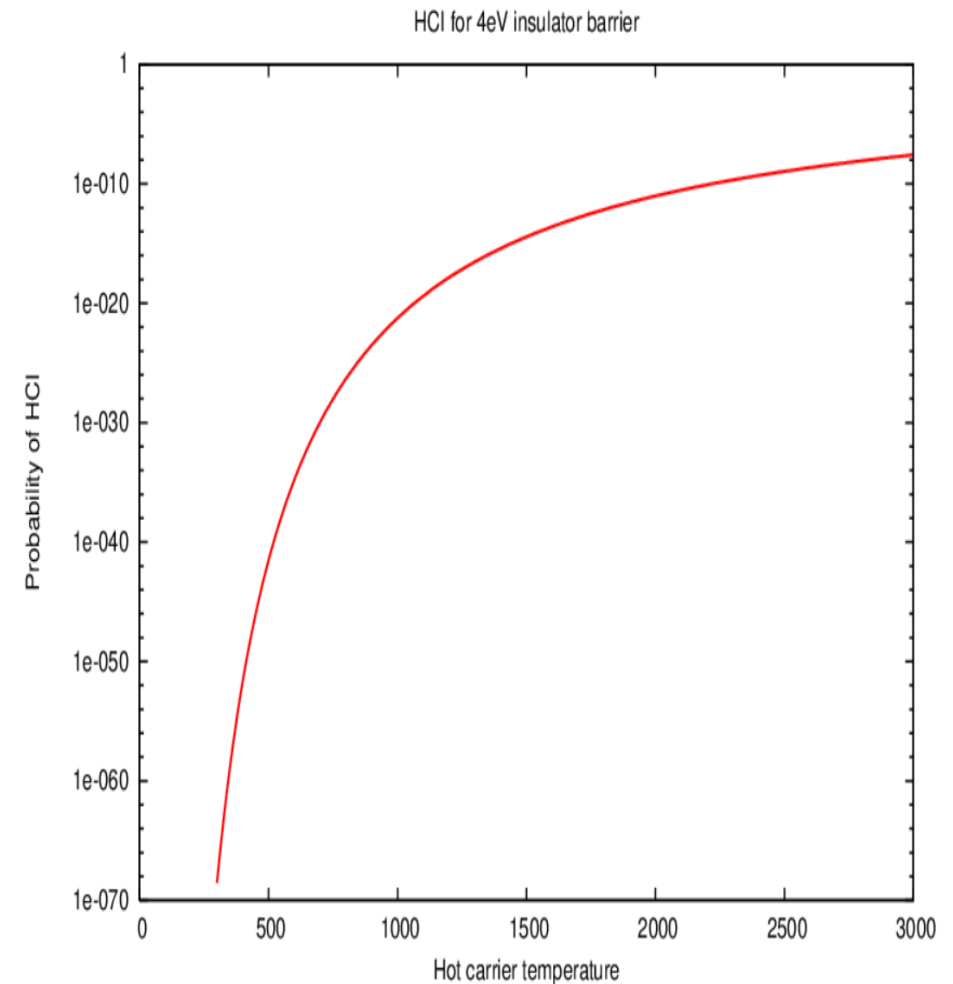
$$\text{prob}(T_e) = \sum_{\text{over } k_y \text{ for } E > E_{ox}} [B \exp(-(E - E_c)/kT_e)]$$

where E is carrier energy, B is normalization constant, E_c is conduction band edge, and E_{ox} is oxide barrier energy. The sum over k_y in k -space can be converted to 1D density of states (DOS) integral and the result can be expressed in $\text{erfc}()$ function.

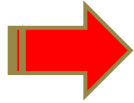
One correction to the above is that hot carrier injecting over the oxide barrier into the poly may not be strictly vertical to the channel and the target may have distribution. Here we assume target of HCI follow a normal distribution of the form:

$$1/\sigma/\sqrt{2\pi} \exp(-0.5*((x-x_0)/\sigma)**2)$$

where σ is the standard deviation and x_0 is the target center.



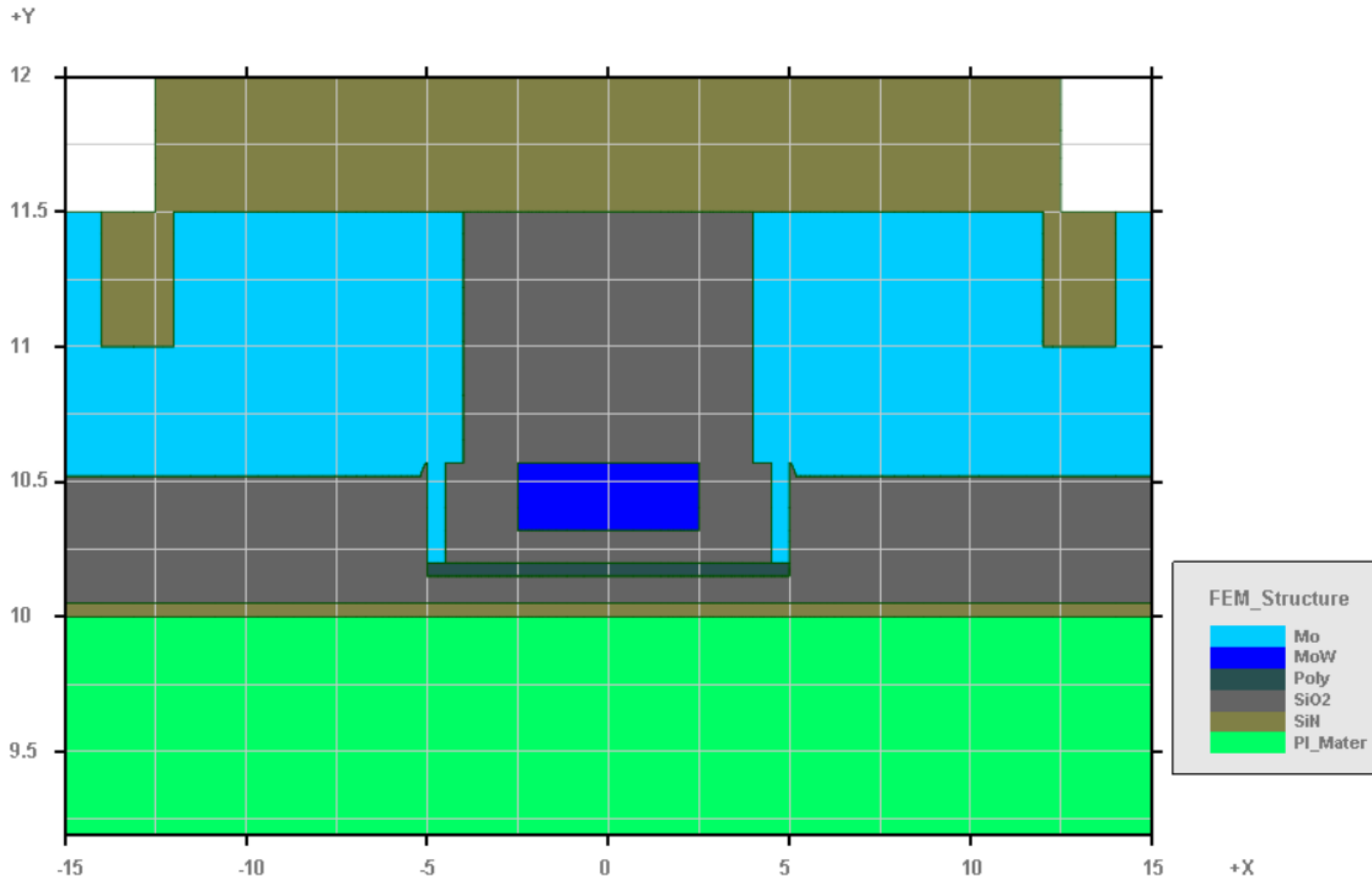
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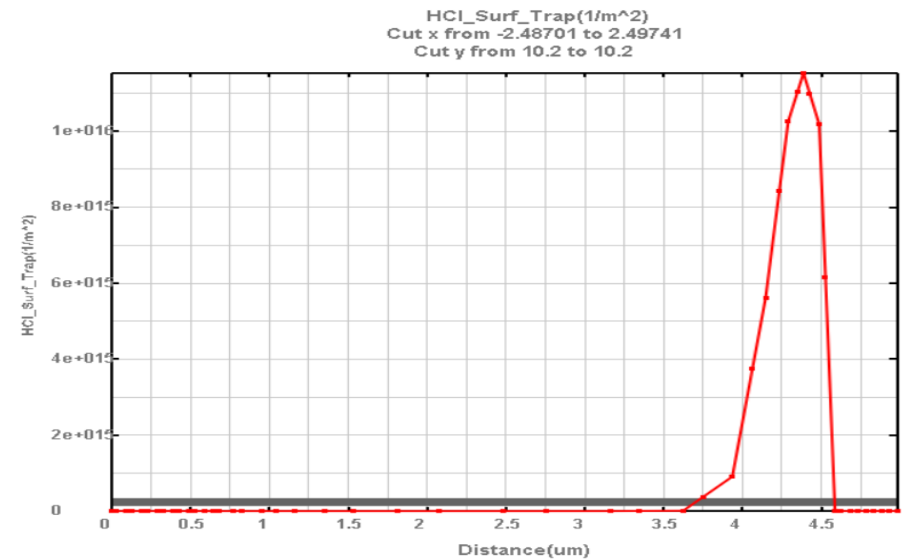
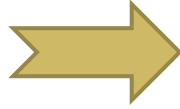
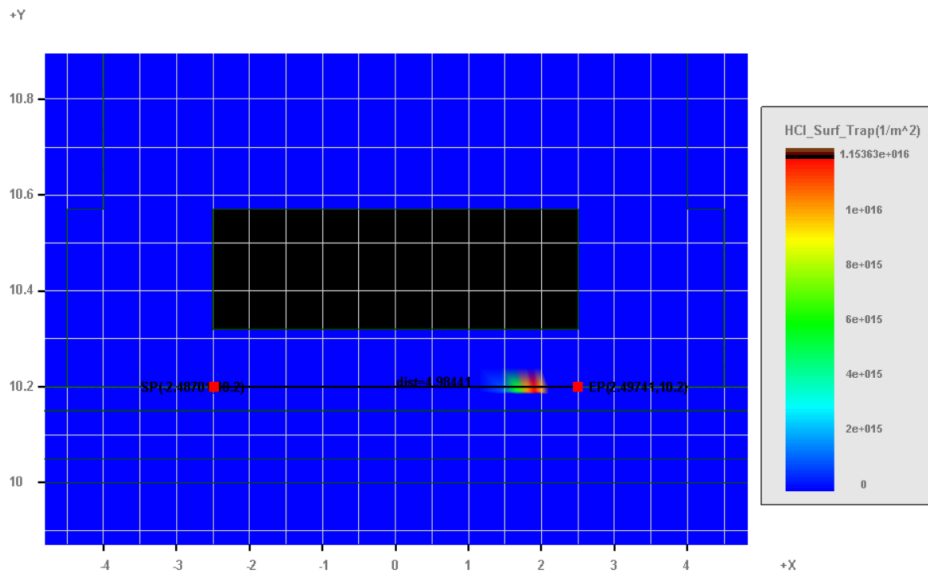
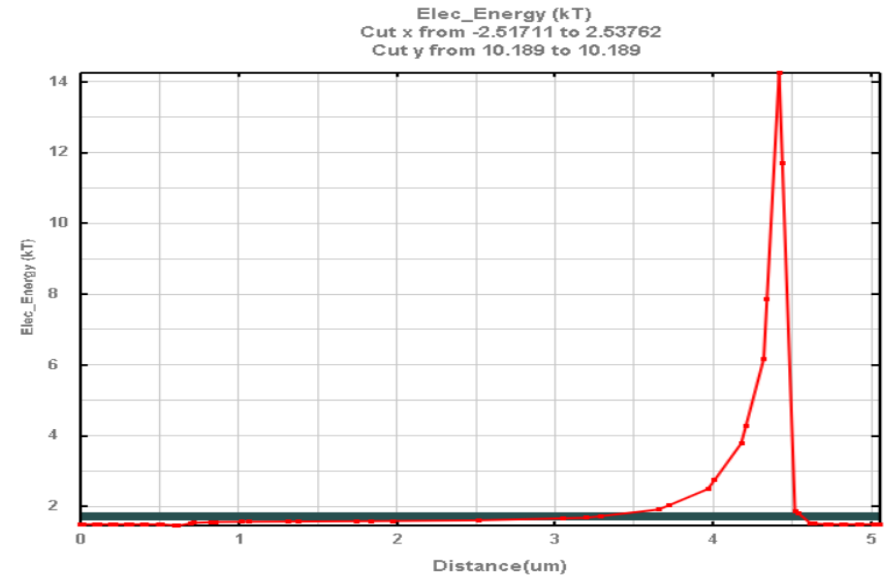
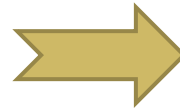
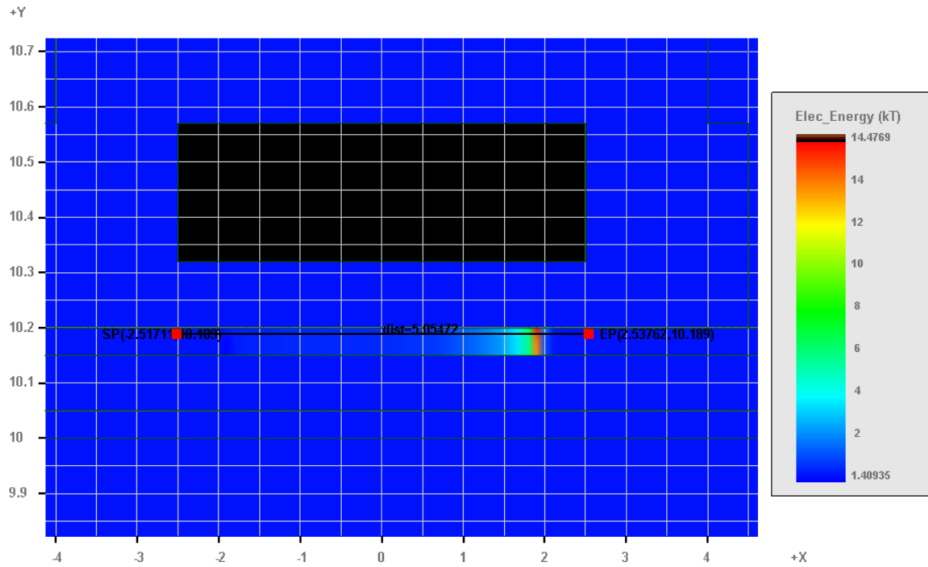
Demo LTPS TFT structure



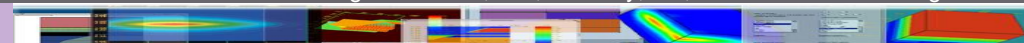
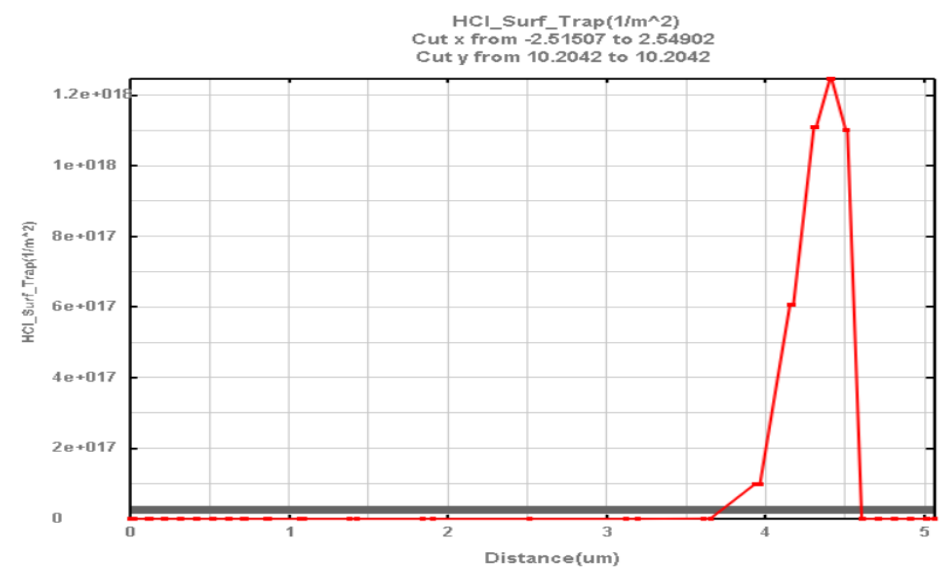
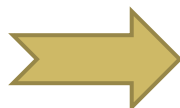
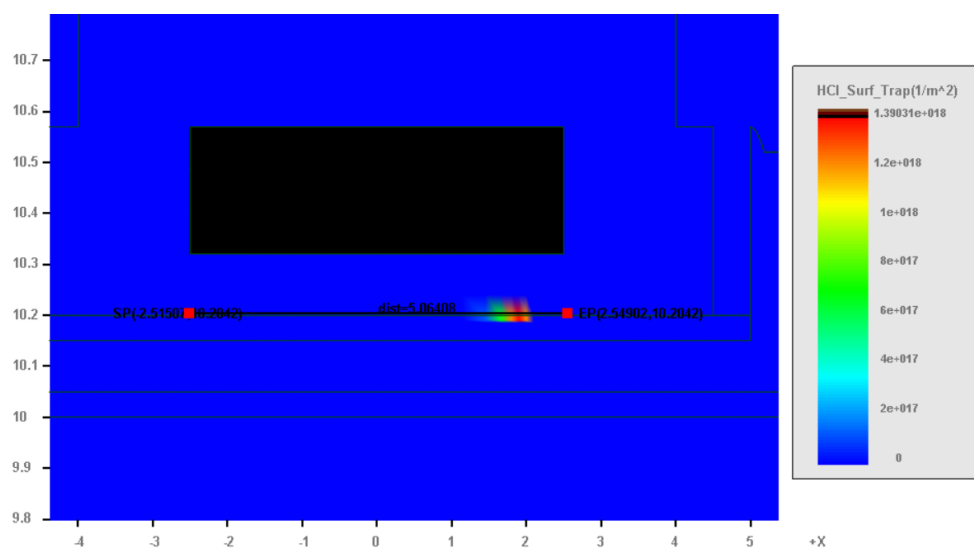
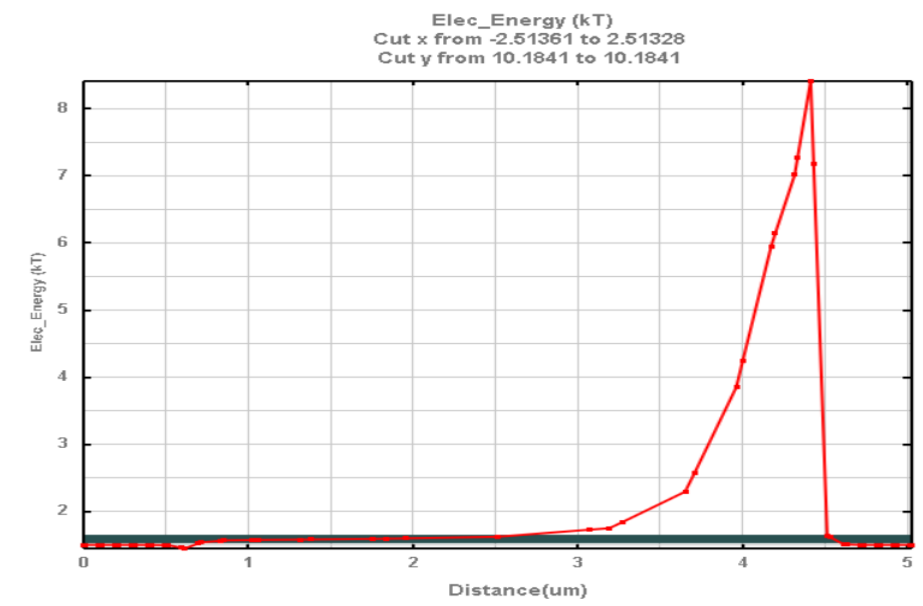
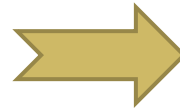
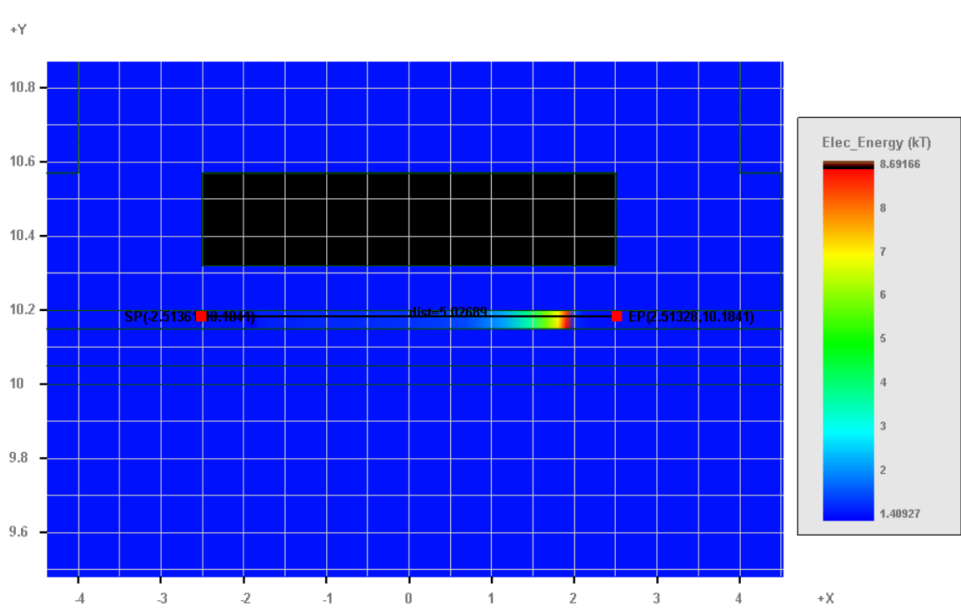
Transient Simulation:

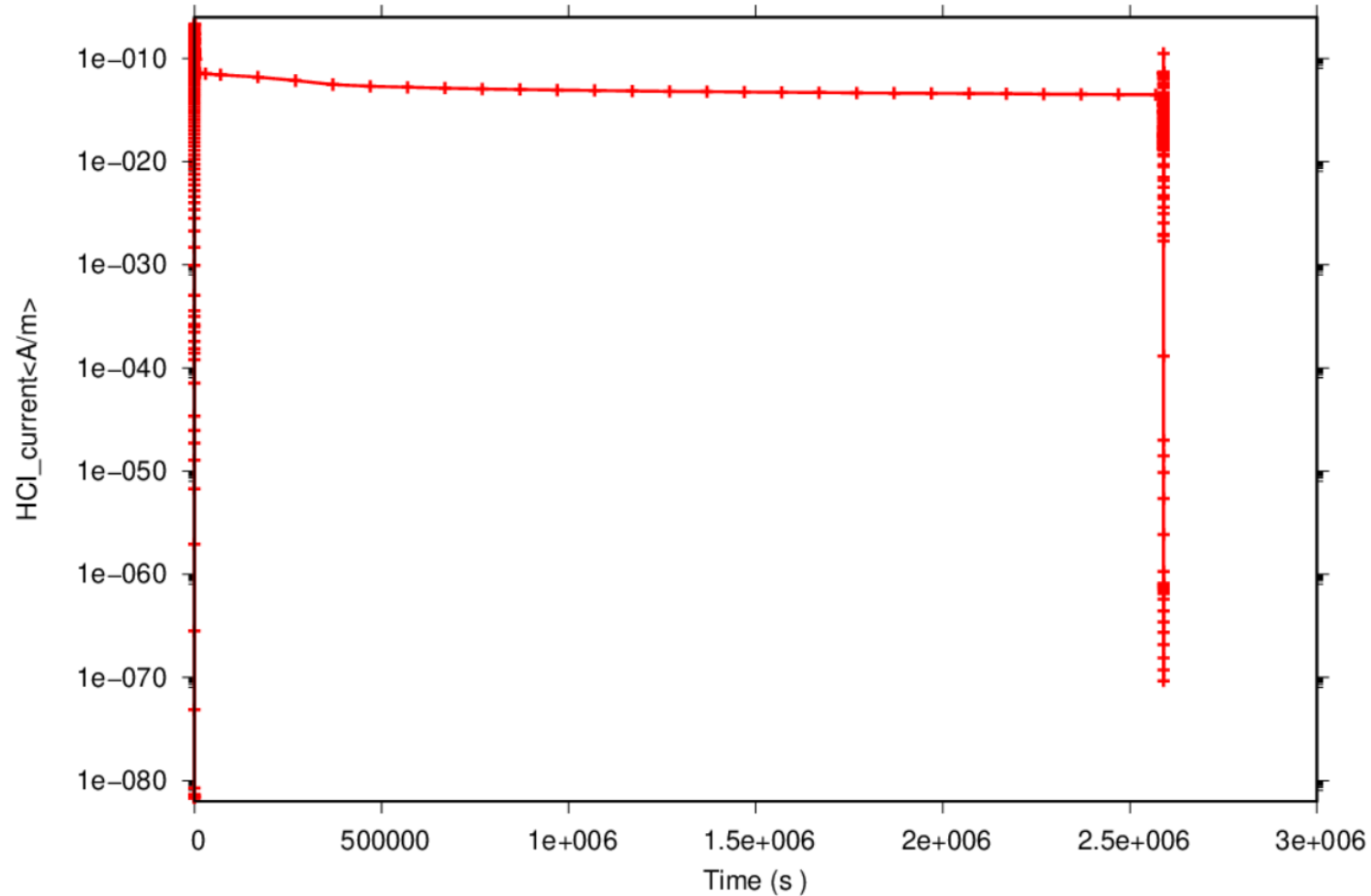
- 1) Using 1sec to ramp up $V_d=10V$ and $V_g=10V$.
- 2) Stay at $V_d=10V$ $V_g=10V$ for one month while studying HCI and HCI generated traps at channel/oxide interface.
- 3) After one month, use 1sec to ramp down V_d V_g and study IV curve to observe any change in threshold voltage

Before long-term high current stress



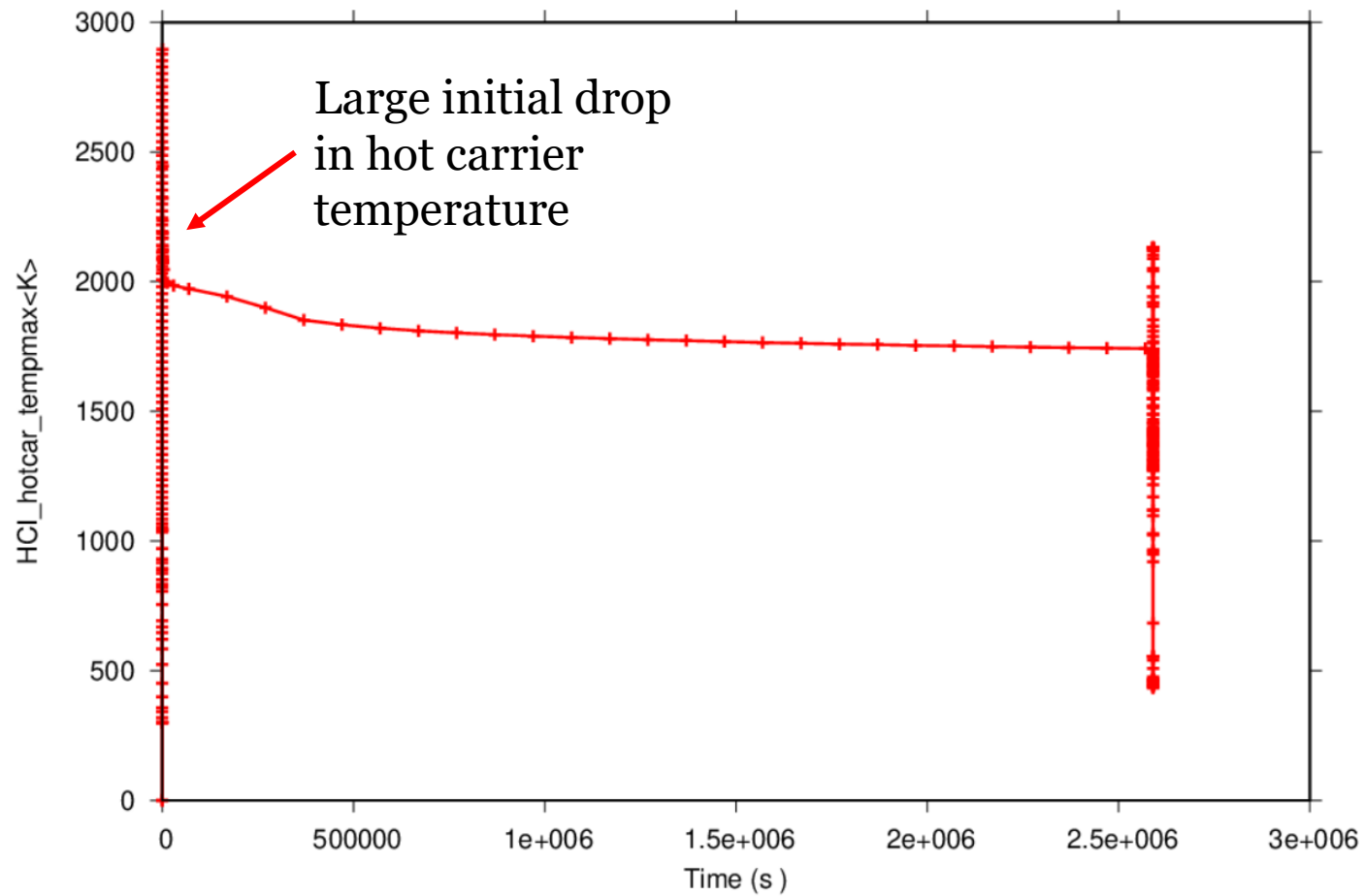
After one-month high current stress





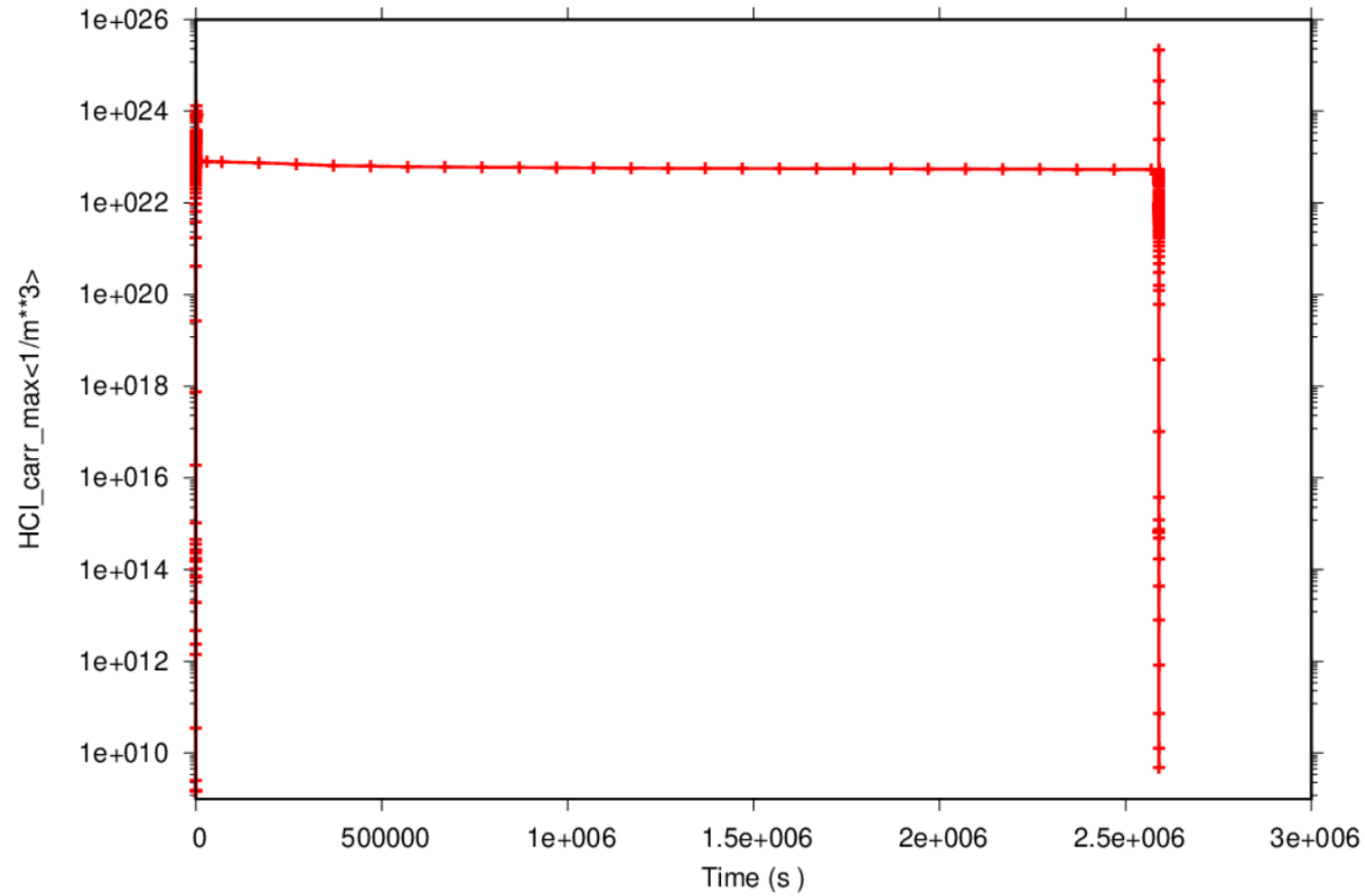
Hot carrier injection (HCI) current into the poly gate varies with stress time, indicating change of electrical potential due to the generation of HCI induced interface defects





Max electron temperature experiences a large initial drop due to the screening of accelerating high field by HCI generated interface traps

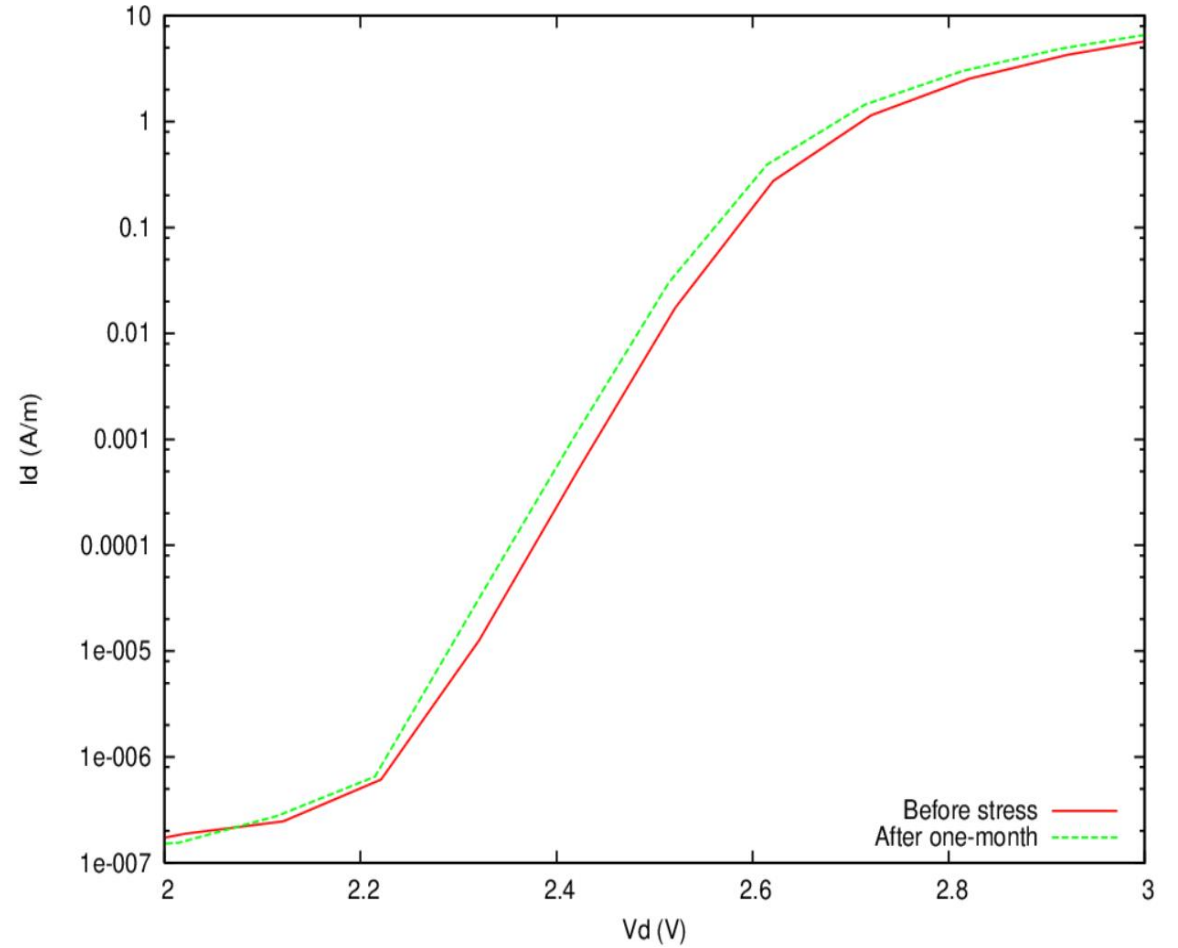
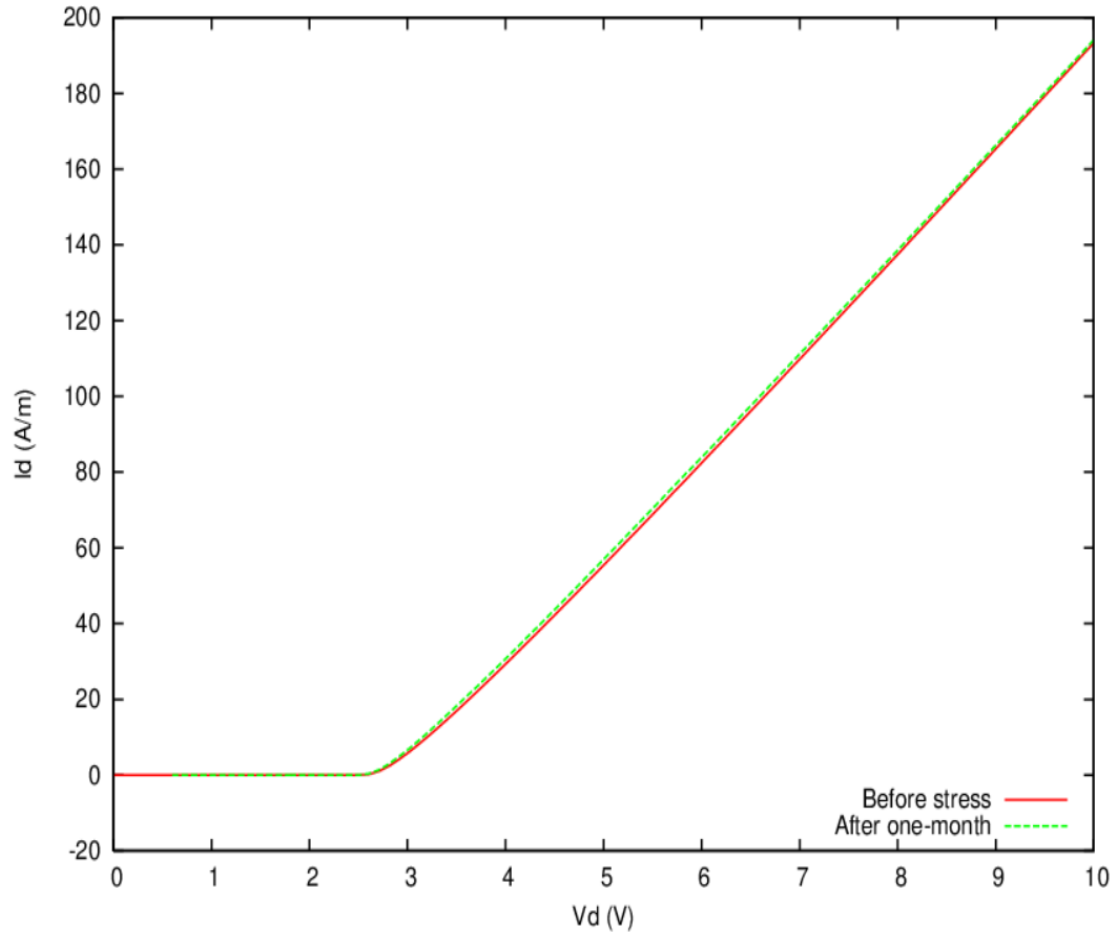




Change of hot-spot carrier concentration indicating variation of electrical potential due to HCI trap generation



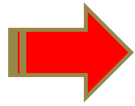
0.03V Vth reduction after one-month of high current stress



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TAD hot carrier model is suitable for reliability analysis.

Interesting to note that HCI induced traps can screen the high stress field and reduce the hot carrier temperature over time.

With reasonable assumption of HCI induced interface traps, V_{th} degradation can be quantified if proper calibration is done.



Thanks for your
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